

# Data analysis, orbit propagation, and the future of MICROSCOPE

Meike List, Stefanie Bremer, Benny Rievers, Hanns Selig

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656<sup>th</sup> WE-Heraeus Seminar “Fundamental Physics in Space”

# Contents

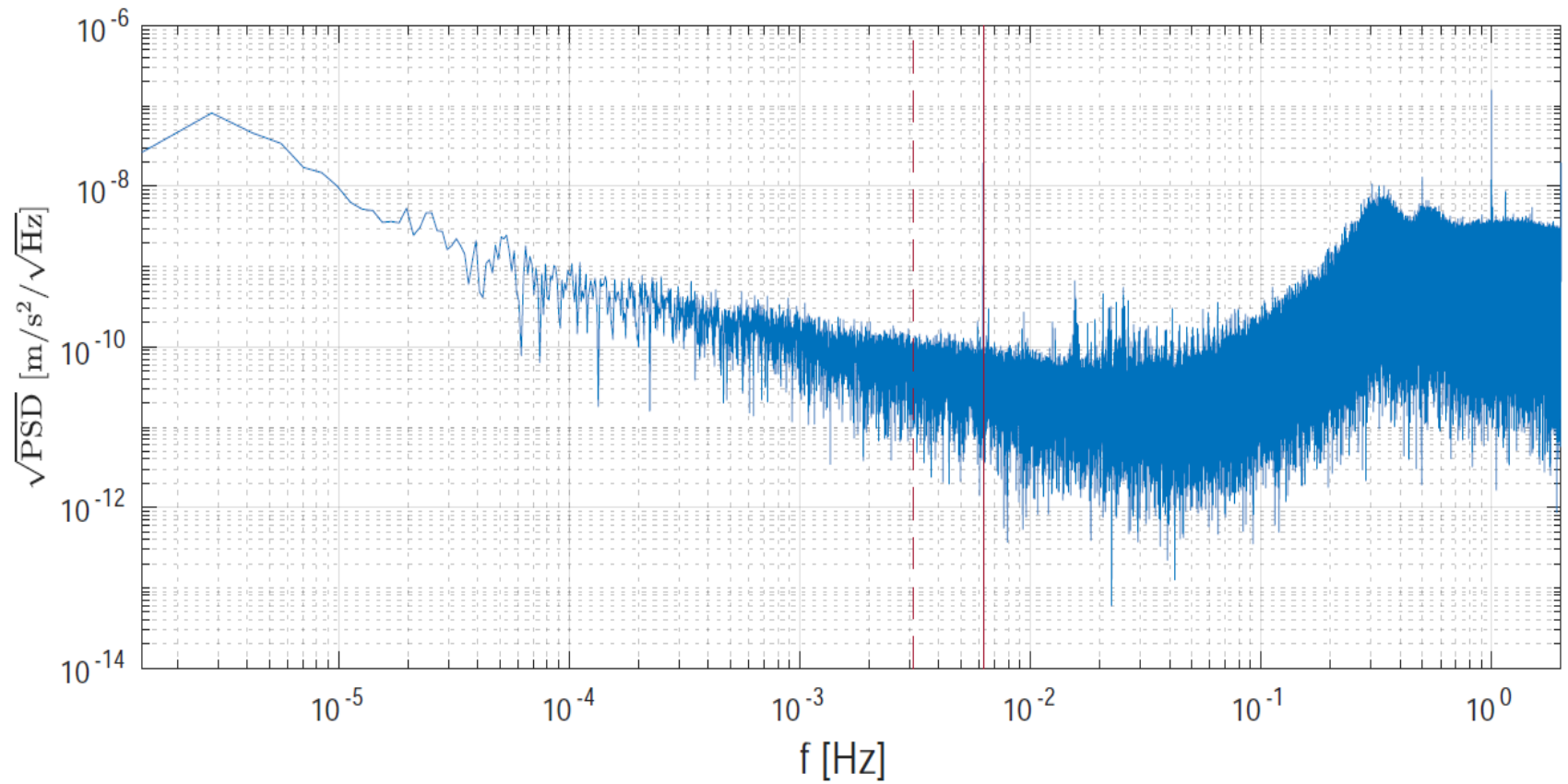
- ✓ Mission data analysis:  
Time-dependent frequency analysis by using wavelets
- ✓ Modeling of non-gravitational disturbances
  - ✓ Motivation
  - ✓ SRP/TRP modeling approach
  - ✓ Example: MICROSCOPE
- ✓ Outlook: post WEP test mission goals
- ✓ Conclusion

# Contents

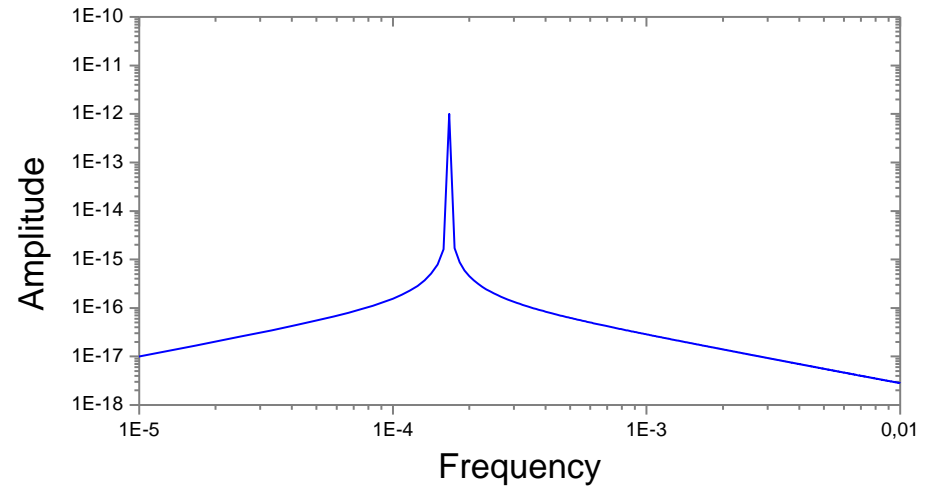
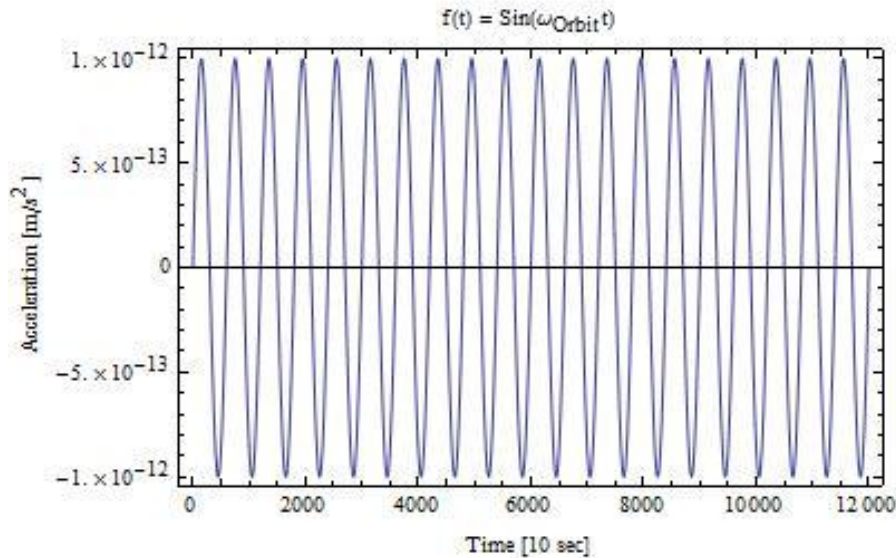
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  - Time-dependent frequency analysis by using wavelets**
  
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# Typical MICROSCOPE acceleration spectrum

## Session with 120 orbits



# Classical frequency analysis



## Limitation

The classical frequency analysis (FT of the complete time signal) shows the best possible frequency resolution

**but** masks any temporal information

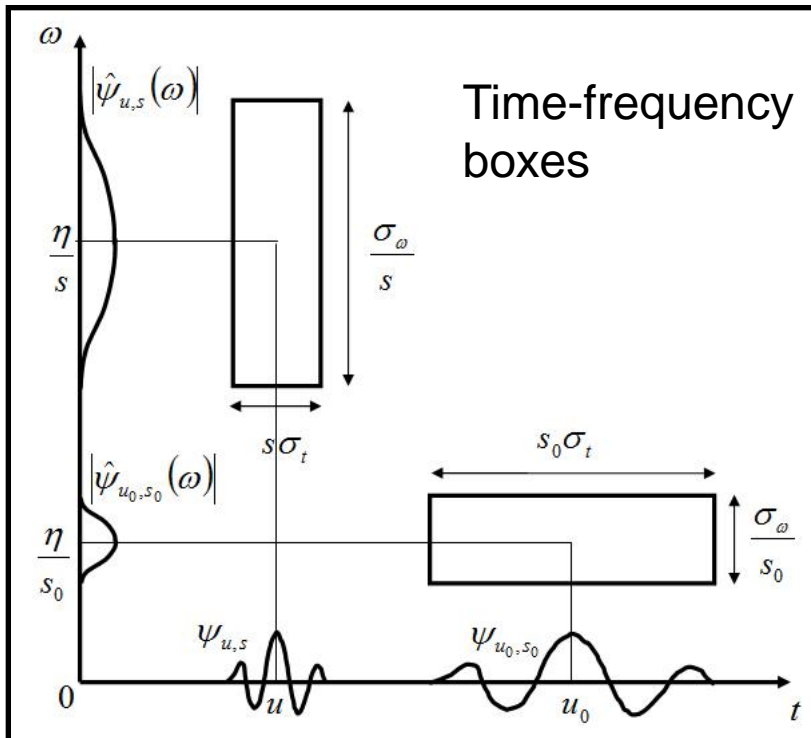
→ best for stationary signals

# Wavelet analysis

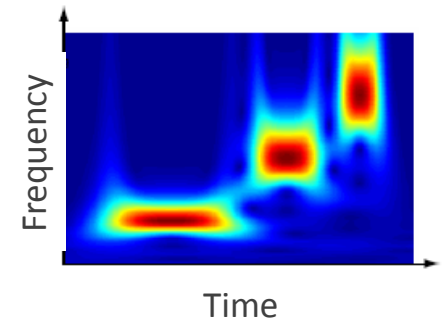
$$WT(u, s) = \frac{1}{\sqrt{|s|}} \int_{-\infty}^{\infty} x(t) \psi * \left( \frac{t-u}{s} \right) dt$$

$u$ : translation  
 $s$ : dilation

$$\int_{-\infty}^{\infty} \psi(t) dt = 0$$



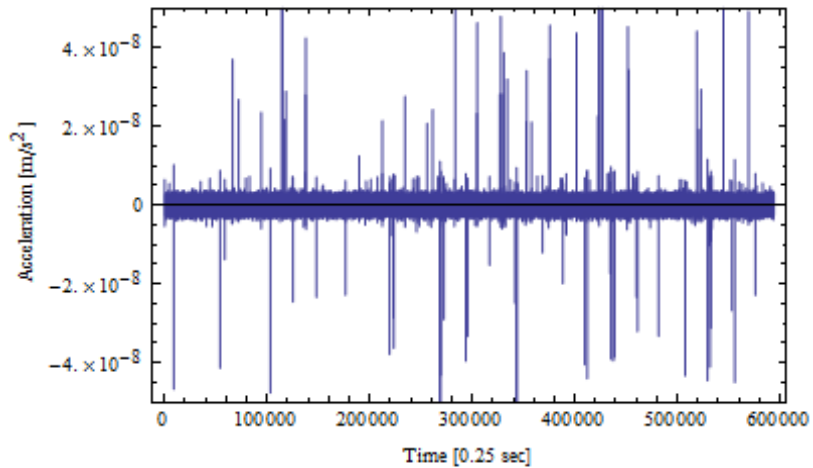
$s_{t,w}$ : uncertainty



recommended Literature: S. Mallet *A wavelet tour of signal processing* Academic Press (1998)

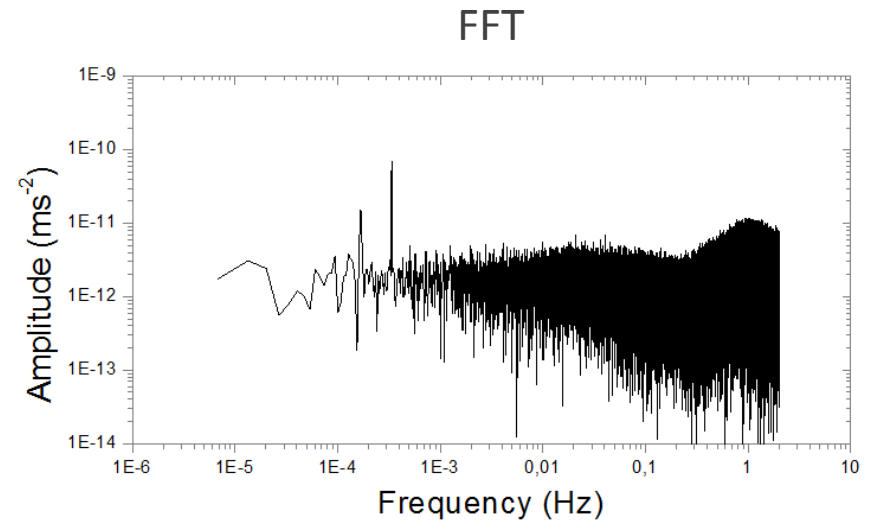
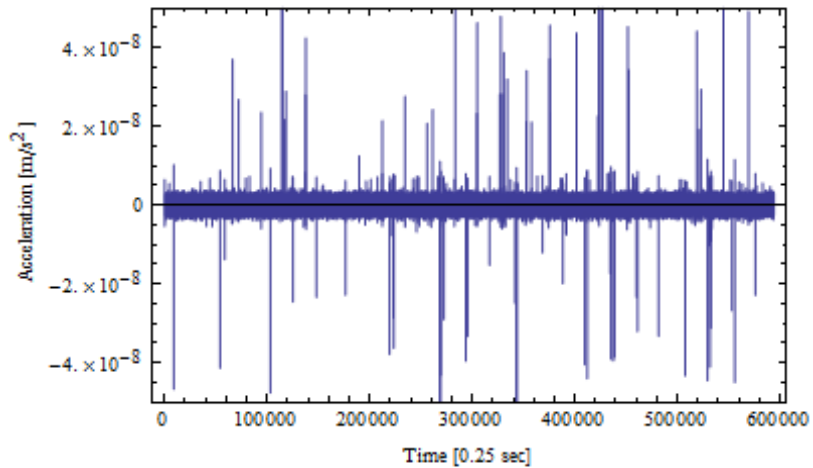
# Example with simulated data set

Simulation: differential acceleration with noise and short time disturbances (spikes)



# Example with simulated data set

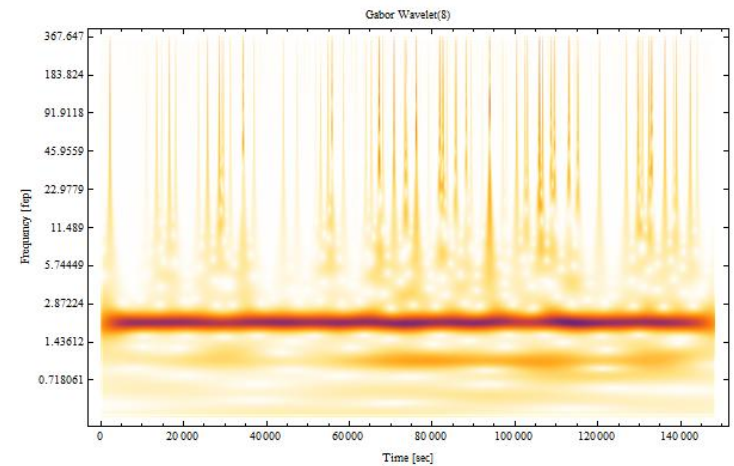
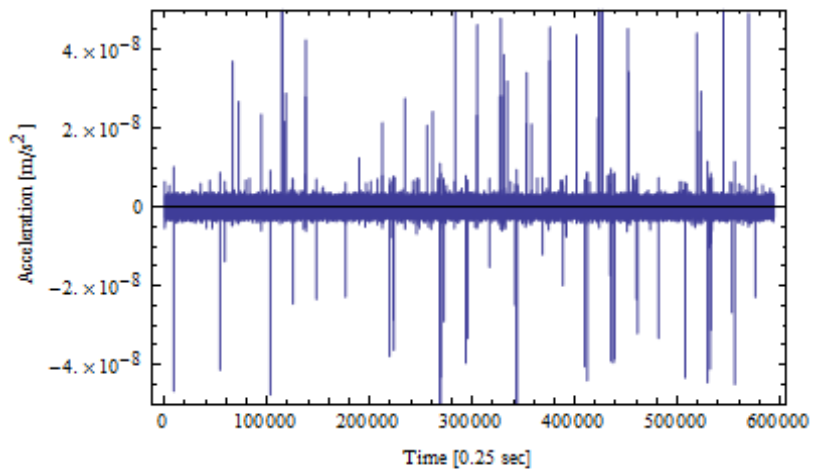
Simulation: differential acceleration with noise and short time disturbances (spikes)






# Example with simulated data set

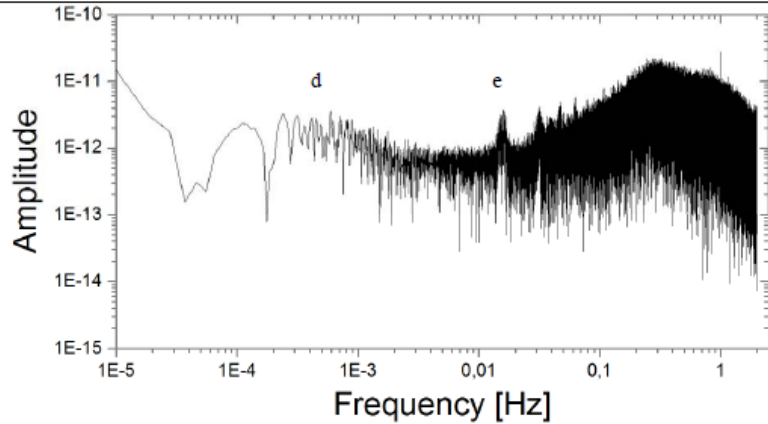
Simulation: differential acceleration with noise and short time disturbances (spikes)



# MICROSCOPE data report example (1st version)

		Ref.: MIC-Data Report Session 80 SUEP IS1- AccXsci Date: 15/10/2016 Page: 10/10
ZARM		

FFT:



Summary:

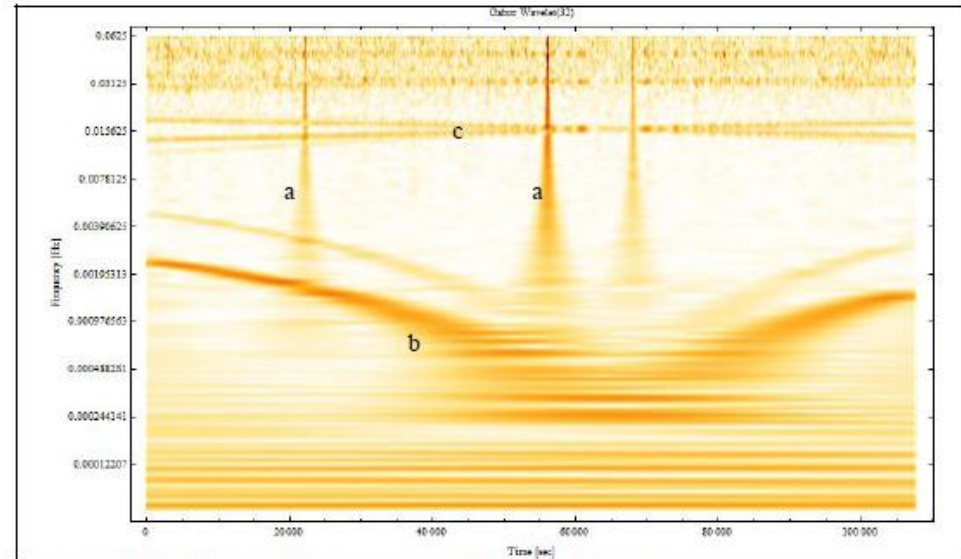
The scalogram of the AccelerationXsci of IS1-SUEP-N1a-Session 80 shows a strange non-stationary behaviour.

The origin of the frequency shifts of the signal (scalogram pattern b, starting at around 2 mHz, then decreasing to 0.2 mHz and then increasing again in a symmetrical way) is not yet understood.

The origin of the other signal component (scalogram pattern c) with crossing lines in the scalograms (mean frequency ~ 15 mHz) is also not yet understood.

It is not yet clear whether the frequency behaviour is based on a real physical effect or on an effect caused by the measurement system (electronics).

		Ref.: MIC-Data Report Session 80 SUEP IS1- AccXsci Date: 16/10/2016 Page: 5/10
Computed and edited by H.Selig and A. Gierse		ZARM



Session 80-N1a\_SUEP\_S-05-IS1-AccXsci minus bias - Scalogram

Ref: Session 80_EPR_V2DFIS1_01_SUEP/N1a_S_05/SUEP/IS1/AccelerationXsci	Remarks: Bias subtracted for the Wavelet analysis to reduce border effects	File: Session 80-N1a_SUEP-S-05-IS1-AccXsci-minus bias.dat	Analysis settings: CWT Gabor (32) Padding -> 0.0
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Description:

Same scalogram but with another setting for frequency/time resolution (Mother wavelet: Gabor(32) -> better frequency resolution, worse time resolution)

# MICROSCOPE data report example (2nd version)

 	Date: April 12, 2017 Page: 3/16
Session_160_EPR_V3DFIS2_01_SUEP	

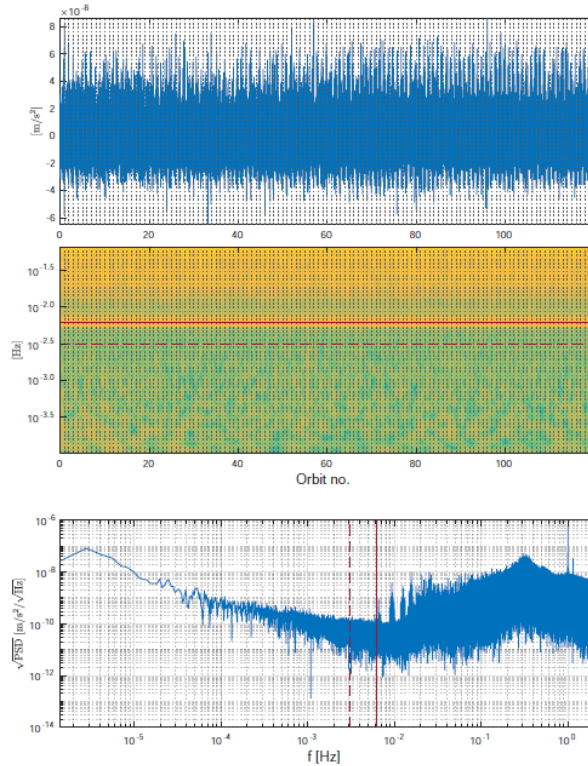




Figure 1: IS1 AccelerationXscaa: Time signal after removing 3rd order polynomial fit, wavelet analysis, and square root of PSD.

 	Date: April 12, 2017 Page: 4/16
Session_160_EPR_V3DFIS2_01_SUEP	

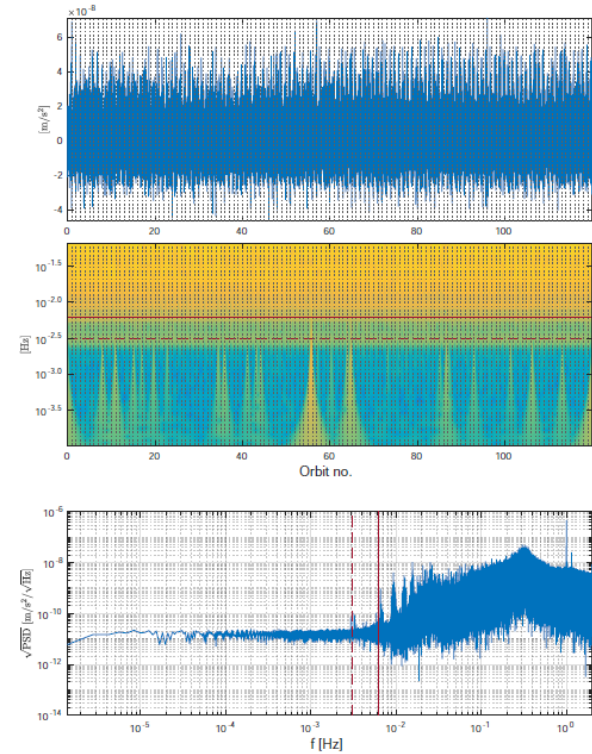
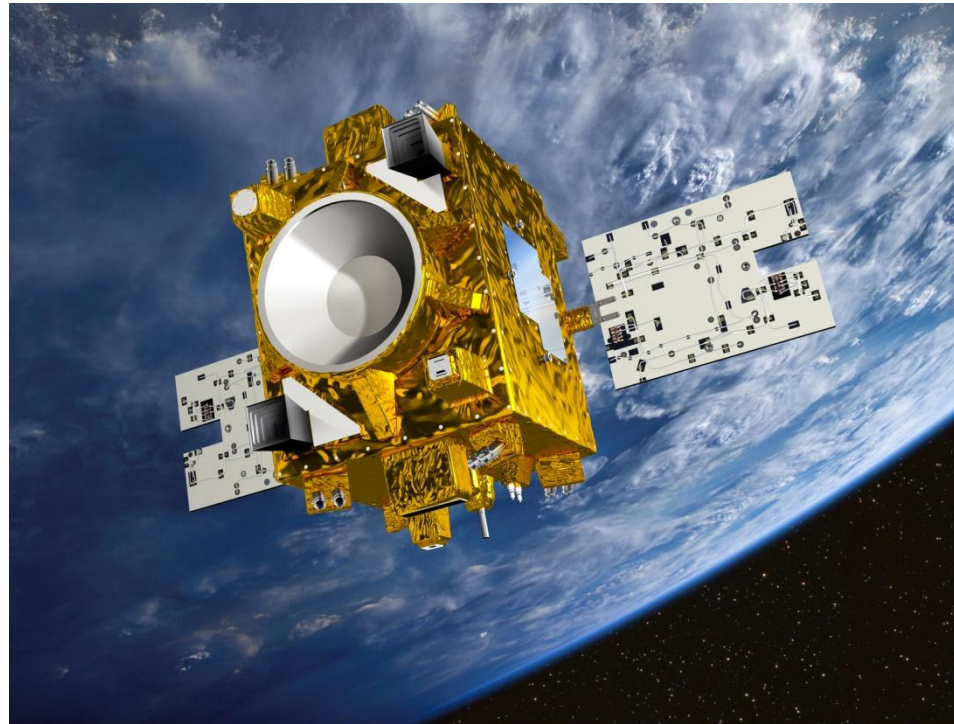


Figure 2: IS2 AccelerationXscaa: Time signal after removing 3rd order polynomial fit, wavelet analysis, and square root of PSD.

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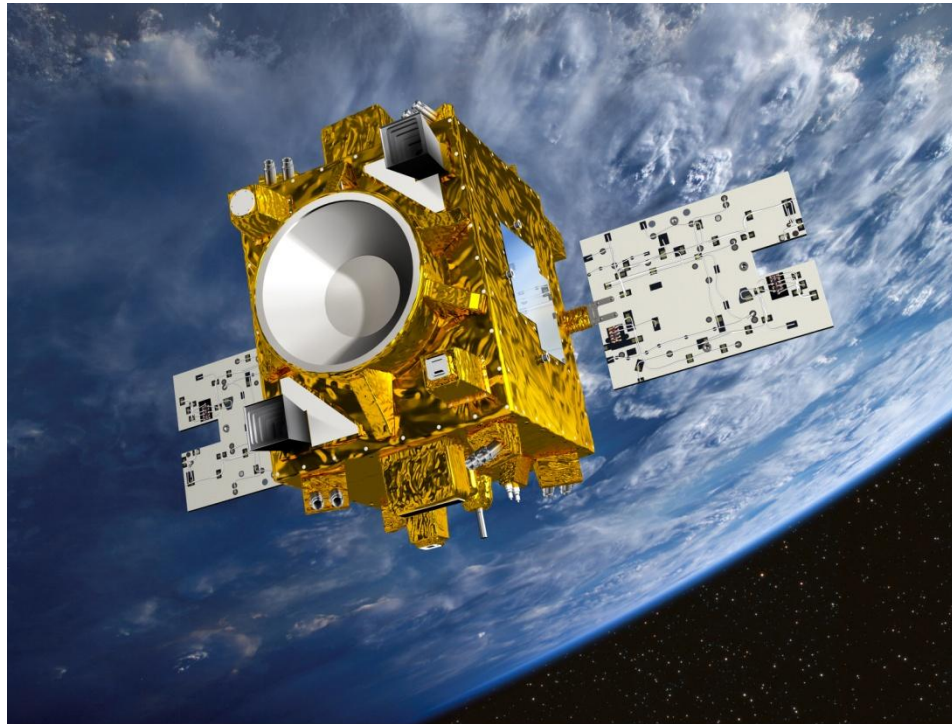
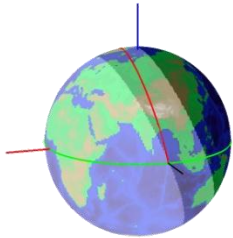
# Motivation: Simulation of satellite missions



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# Motivation: Simulation of satellite missions

Orbit dynamics

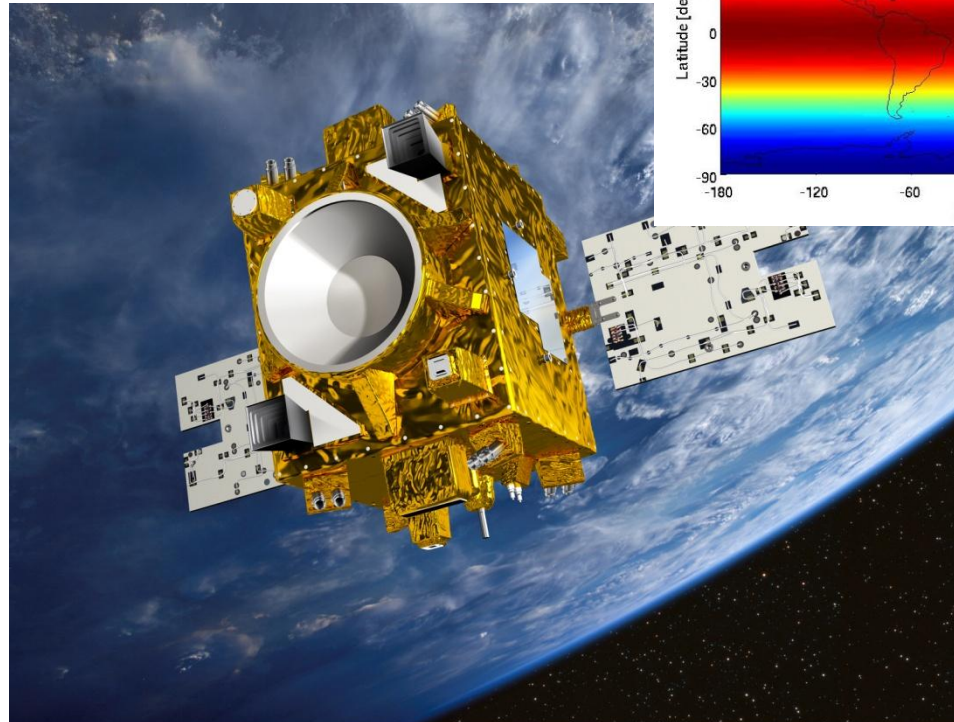
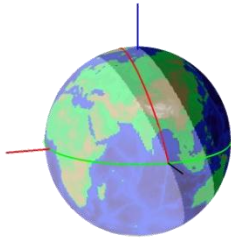


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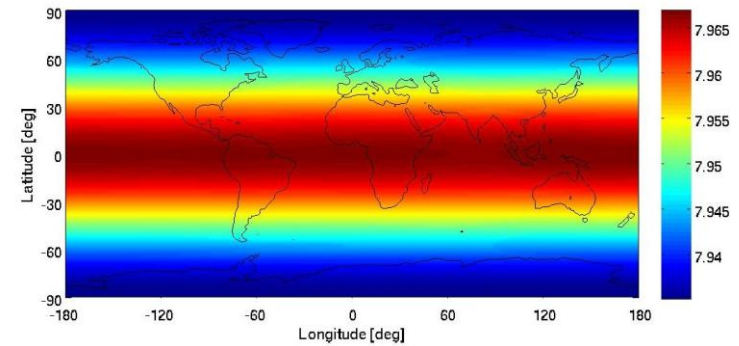
# Motivation: Simulation of satellite missions

## Gravity field of the Earth

Orbit dynamics

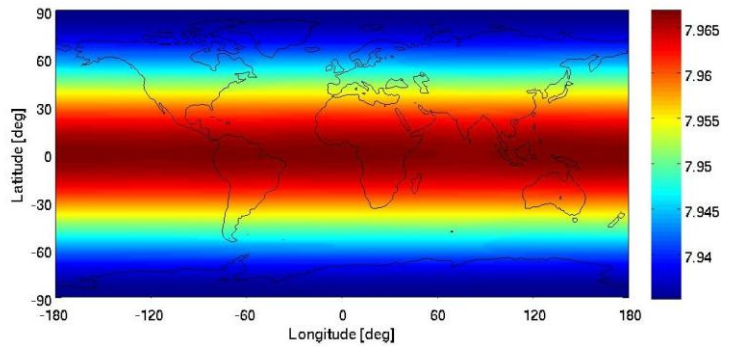


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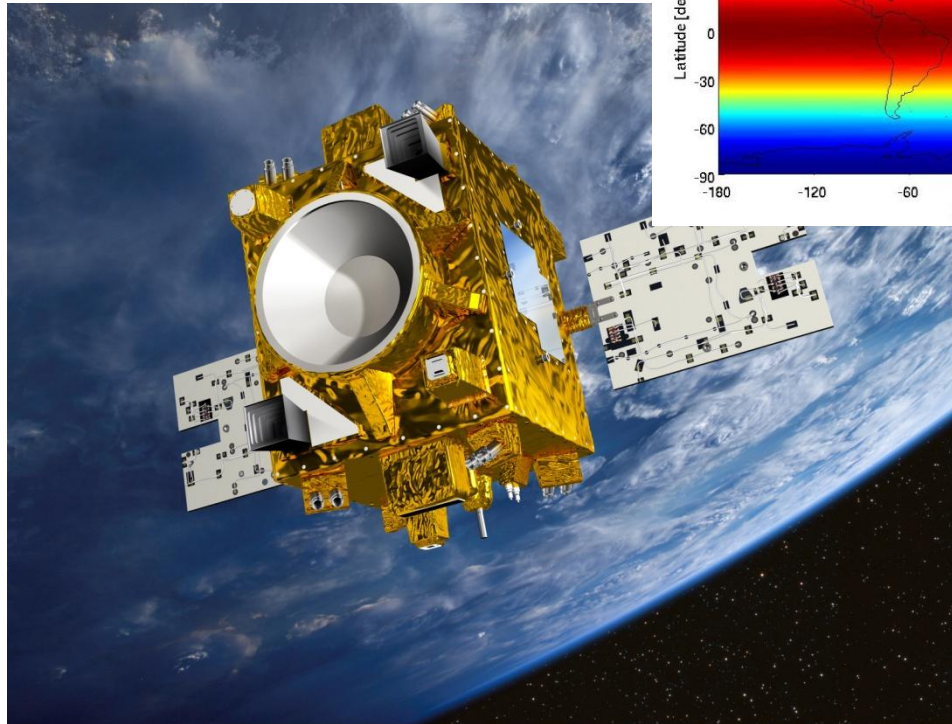
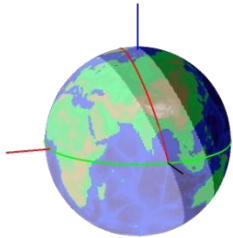


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## Gravity field of the Earth

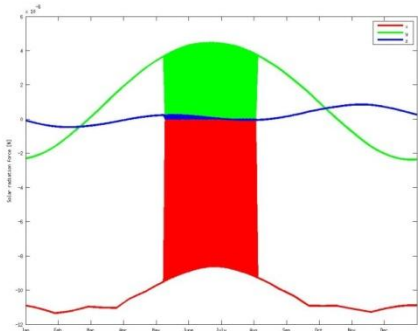


## Orbit dynamics



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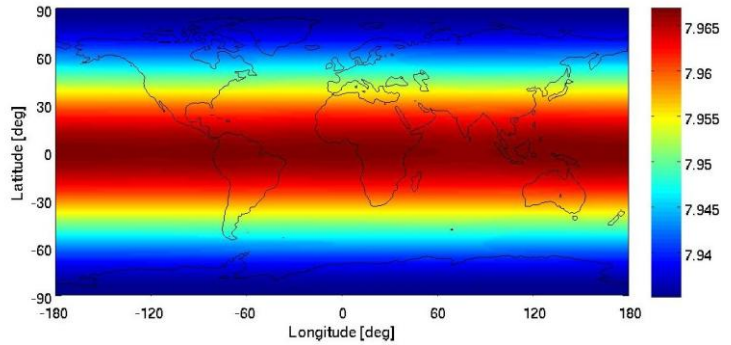
## Solar radiation pressure and eclipse



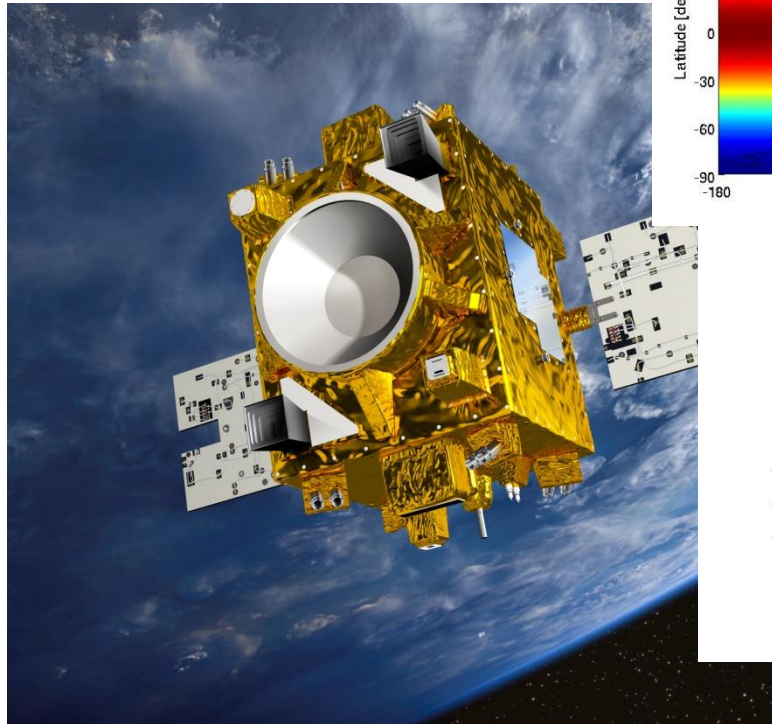
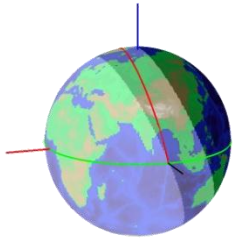


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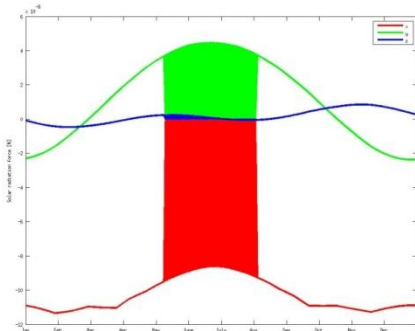


## Orbit dynamics

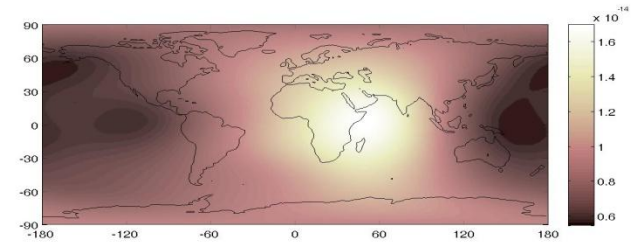


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## Solar radiation pressure and eclipse

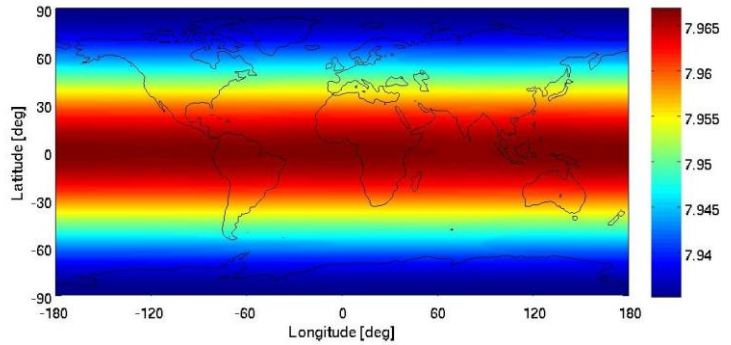


## Atmosphere

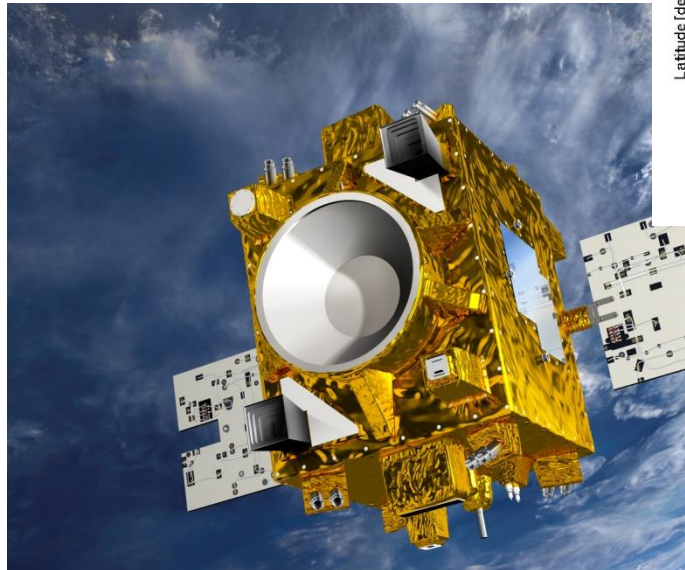
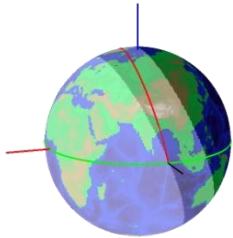


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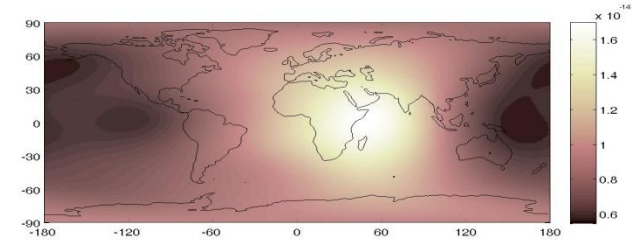
## Gravity field of the Earth



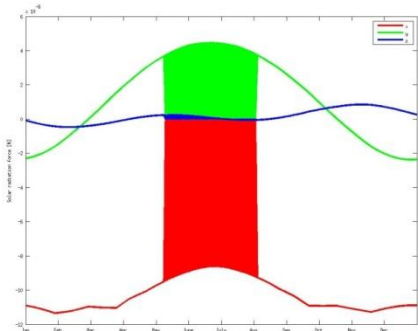
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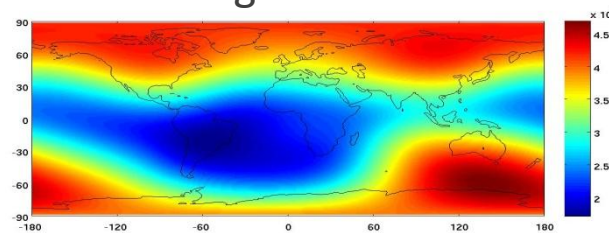
## Atmosphere



## Solar radiation pressure and eclipse

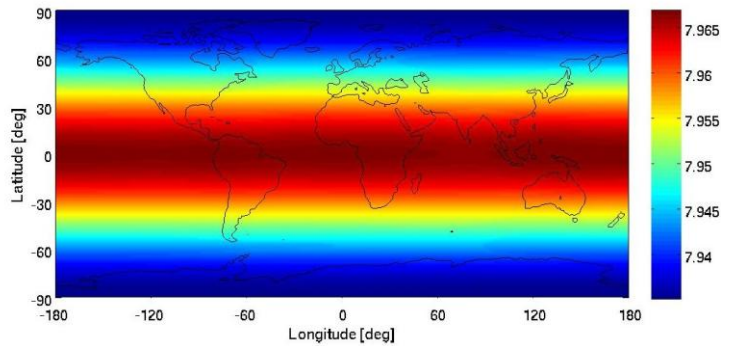


## Magnetic field

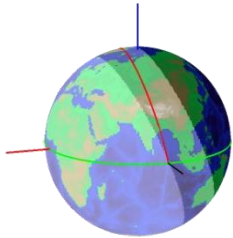


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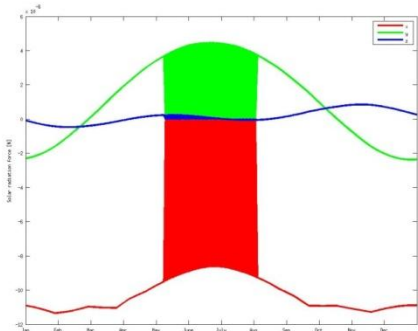
## Gravity field of the Earth



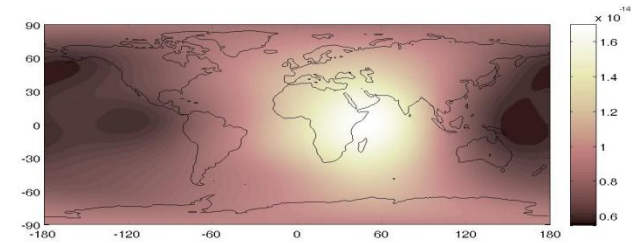
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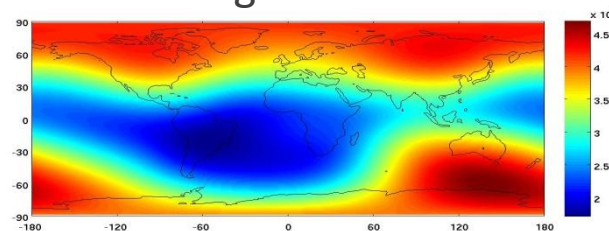
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## Atmosphere



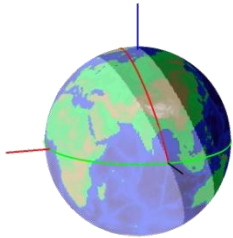
## Magnetic field



- ✓ Albedo radiation
- ✓ Earth infrared radiation
- ✓ Space debris
- ✓ Ephemerides
- ✓ ...

# Motivation: Simulation of satellite missions

Orbit dynamics

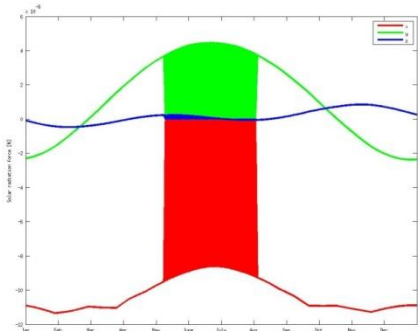


Special requirement of mission:

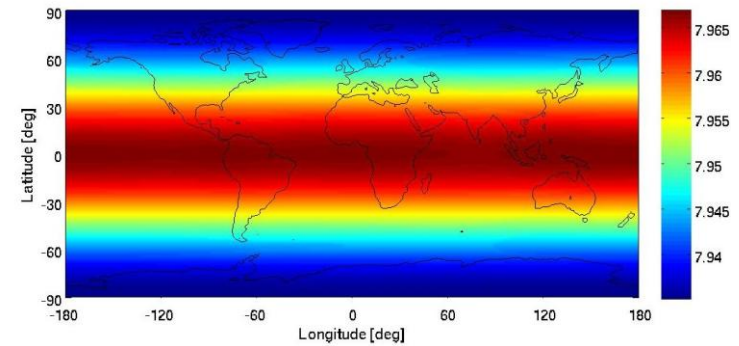
**Payload**



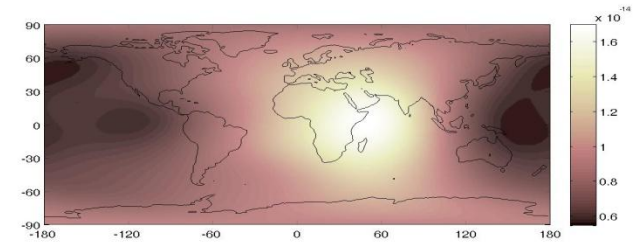
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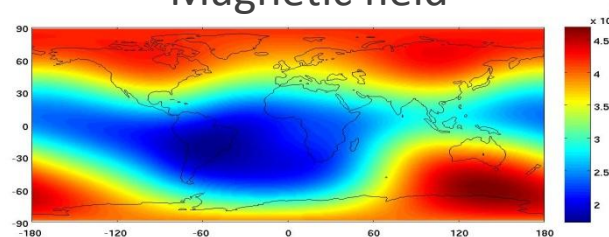
Gravity field of the Earth



Atmosphere



Magnetic field

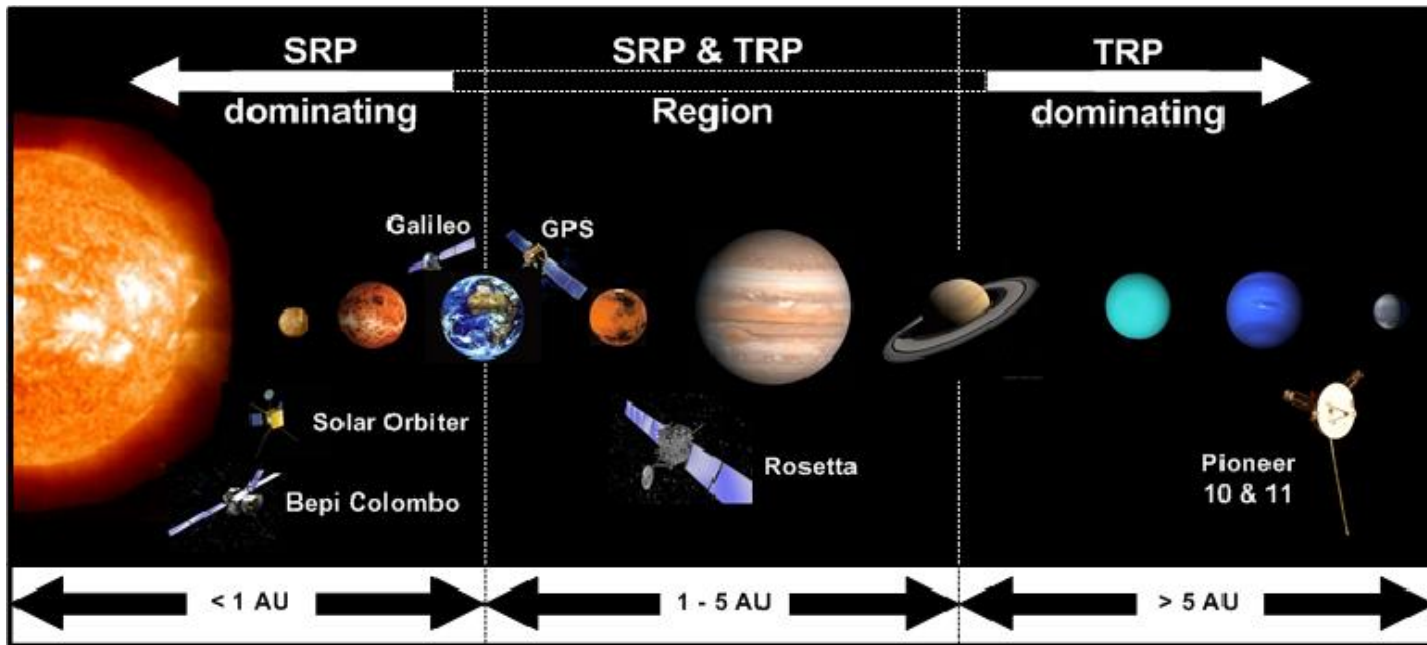


- ✓ Albedo radiation
- ✓ Earth infrared radiation
- ✓ Space debris
- ✓ Ephemerides
- ✓ ...

# Motivation

- ✓ Central task for mission analysis:
  - Modeling and propagation of the real mission orbit
  - initial conditions and modeling of space environment
  
- ✓ Satellite motion in the gravitational field of the Earth
  - non-uniform mass distribution (zonal and tesseral variations), Earth oblateness
  - non-spherically symmetric Earth gravitational field results in „gravitational disturbances“ of the pure Keplerian orbit
  
- ✓ „Non-gravitational disturbances“ have a large effect on satellite motion and its attitude
  - Atmospheric drag due to residual atmosphere
    - T. Kato, B. Rievers, M. List, Trans. JSASS Aerospace Tech. Japan Vol. 14, No. ists30, 2016
  - Solar radiation pressure (SRP) and Thermal radiation pressure (TRP)
    - M. List, S. Bremer, B. Rievers, H. Selig, Int. Journal Aerospace Eng., Vol. 2015, 928206, 2015
    - B. Rievers, M. List and S. Bremer, Adv. Astro. Sci. 158, 2997 – 3012, 2016

# Motivation



- ✓ Implementation of TRP model in ESOC Orbit Determination Software based on study of method for modeling satellite surface forces with application to Rosetta  
→ Correction of implemented SRP model

B. Rievers, T. Kato, J. C. van der Ha, and C. Lämmerzahl, Adv. Astro. Sci. 143 1123-1142, 2012

- ✓ Pioneer Anomaly: TRP effect

B. Rievers, C. Lämmerzahl, Ann. Phys. 523 (6), 439-449, 2011

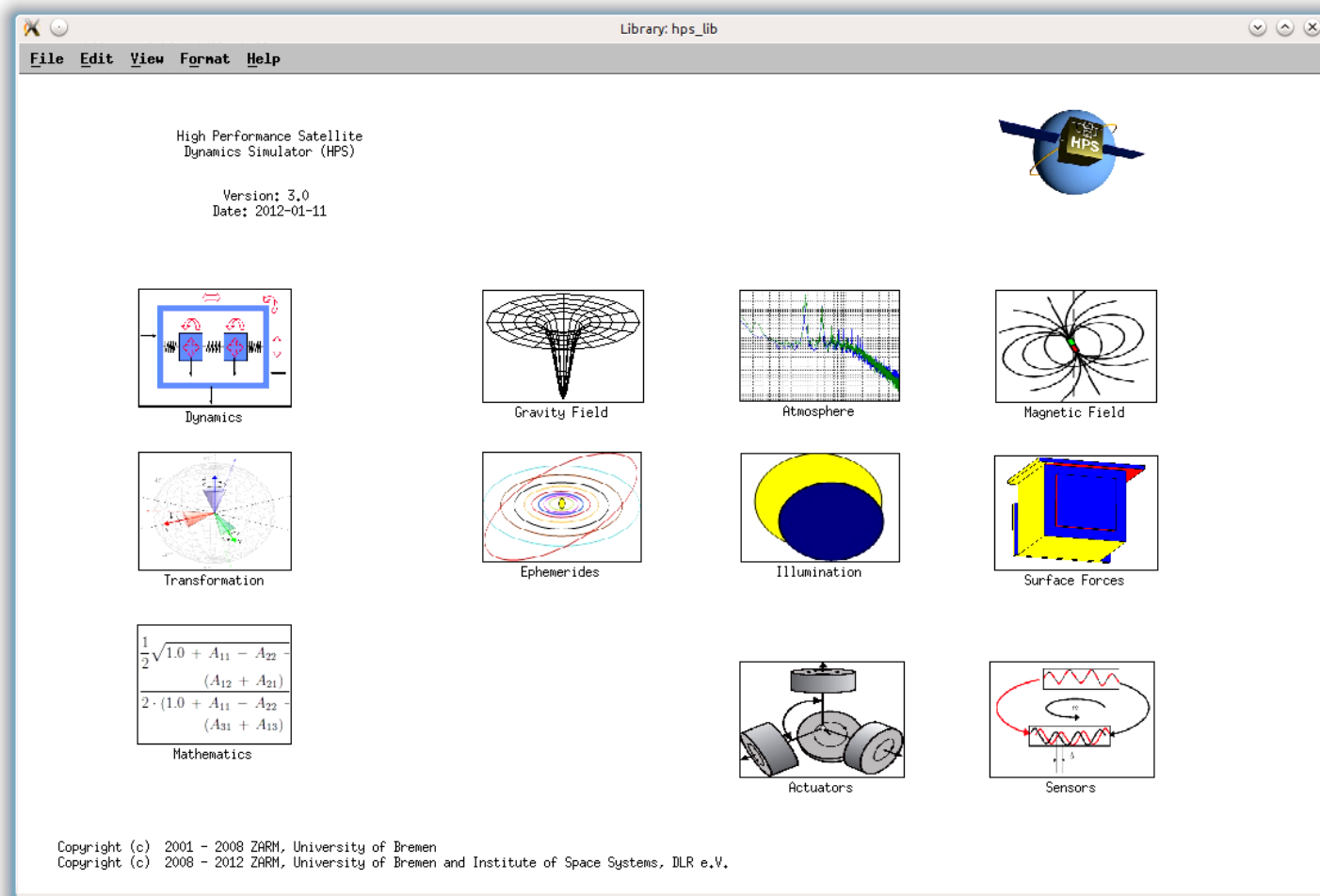
B. Rievers, S. Bremer, M. List, C. Lämmerzahl, H. Dittus, Acta. Astro. 66 (3-4), 467-476, 2010

B. Rievers, C. Lämmerzahl, M. List, S. Bremer, and H. Dittus, New J. Phys. 11 113032, 2009

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# High Performance Satellite Dynamics Simulator





# High Performance Satellite Dynamics Simulator

High Performance Satellite Dynamics Simulator (HPS)

Version: 3.0  
Date: 2012-01-11

**satellite and test mass dynamics**

Dynamics Gravity Field

**environment models and computation of resulting forces and torques**

Atmosphere Magnetic Field

**mathematics**

Transformation

Mathematics

$$\frac{1}{2} \sqrt{1.0 + A_{11} - A_{22}}$$
$$(A_{12} + A_{21})$$
$$2 \cdot (1.0 + A_{11} - A_{22} - (A_{31} + A_{13}))$$

**sensors and actuators**

Actuators Sensors

Copyright (c) 2001 - 2008 ZARM, University of Bremen  
Copyright (c) 2008 - 2012 ZARM, University of Bremen and Institute of Space Systems, DLR e.V.

# Modeling of solar radiation pressure

Differential radiation force due to

✓ Absorption:  $d\vec{F}_\alpha = -P\alpha \cos(\theta)\vec{e}_{\text{Sun}}dA$

✓ Specular reflection:  $d\vec{F}_{\gamma_S} = -2P\gamma_S \cos^2(\theta)\vec{e}_N dA$

✓ Diffuse reflection:  $d\vec{F}_{\gamma_D} = P\gamma_D \left( -\frac{2}{3} \cos(\theta)\vec{e}_N - \cos(\theta)\vec{e}_{\text{Sun}} \right) dA$

Resulting force:  $\vec{F}_{\text{solar}} = \sum_i \vec{F}_i$

with

$$\vec{F}_i = \int d\vec{F}_{\text{total}} = -P \int \left[ (1 - \gamma_S) \vec{e}_{\text{Sun}} + 2 \left( \gamma_S \cos(\theta) + \frac{1}{3} \gamma_D \right) \vec{e}_N \right] \cos(\theta) dA$$

# Modeling of solar radiation pressure

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Geometry



# Modeling of solar radiation pressure

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Resulting force:  $\vec{F}_{\text{solar}} = \sum_i \vec{F}_i$

with

Material degradation (BOL  $\leftrightarrow$  EOL)

Geometry

$$\vec{F}_i = \int d\vec{F}_{\text{total}} = -P \int \left[ (1 - \gamma_S) \vec{e}_{\text{Sun}} + 2 \left( \gamma_S \cos(\theta) + \frac{1}{3} \gamma_D \right) \vec{e}_N \right] \cos(\theta) dA$$

# Modeling of thermal radiation pressure

- ✓ Resulting surface temperature: 
$$T_i = \sqrt[4]{\frac{P_{\odot,i} P_i}{\sigma A_i \varepsilon_i}}$$
- ✓ Actual mean solar constant: 
$$P_{\odot,i} = \frac{P_{\odot,1AU}}{r^2} \alpha_i \cos(\xi_i)$$
- ✓ Actual orientation angle: 
$$\xi_i = \arccos(\vec{e}_{N,i} \cdot \vec{e}_{Sun})$$

Resulting TRP force vector of each cell:

$$\vec{F}_{TRP,i} = -\frac{2}{3} \vec{e}_{N,i} A_i \frac{P_{\odot,i} + P_i}{c}$$

# Modeling of thermal radiation pressure

- ✓ Resulting surface temperature:  $T_i = \sqrt[4]{\frac{P_{\odot,i} P_i}{\sigma A_i \varepsilon_i}}$
- ✓ Actual mean solar constant:  $P_{\odot,i} = \frac{P_{\odot,1AU}}{r^2} \alpha_i \cos(\xi_i)$
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Resulting TRP force vector of each cell:

Geometry

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# Modeling of thermal radiation pressure

✓ Resulting surface temperature: 
$$T_i = \sqrt[4]{\frac{P_{\odot,i} P_i}{\sigma A_i \varepsilon_i}}$$

✓ Actual mean solar constant: 
$$P_{\odot,i} = \frac{P_{\odot,1AU}}{r^2} \alpha_i \cos(\xi_i)$$

Material degradation (BOL  $\leftrightarrow$  EOL)

✓ Actual orientation angle: 
$$\xi_i = \arccos(\vec{e}_{N,i} \cdot \vec{e}_{Sun})$$

Resulting TRP force vector of each cell:

Geometry

$$\vec{F}_{TRP,i} = -\frac{2}{3} \vec{e}_{N,i} A_i \frac{P_{\odot,i} + P_i}{c}$$

# Material degradation influence

- ✓ Assumption: surface degradation leads to microscopic cratering  
→ increase of absorptivity due to increase of surface area (resulting from roughened surface)

$$\frac{d\alpha}{dt} = p \frac{1}{t} \implies \alpha = \alpha_{\text{BOL}} + \frac{p}{\ln(t)}, \quad p = \frac{\alpha_{\text{EOL}} - \alpha_{\text{BOL}}}{\ln(T_{\text{lifetime}})}$$

- ✓ Roughening of surfaces changes ratio between spectral and diffuse reflectivity

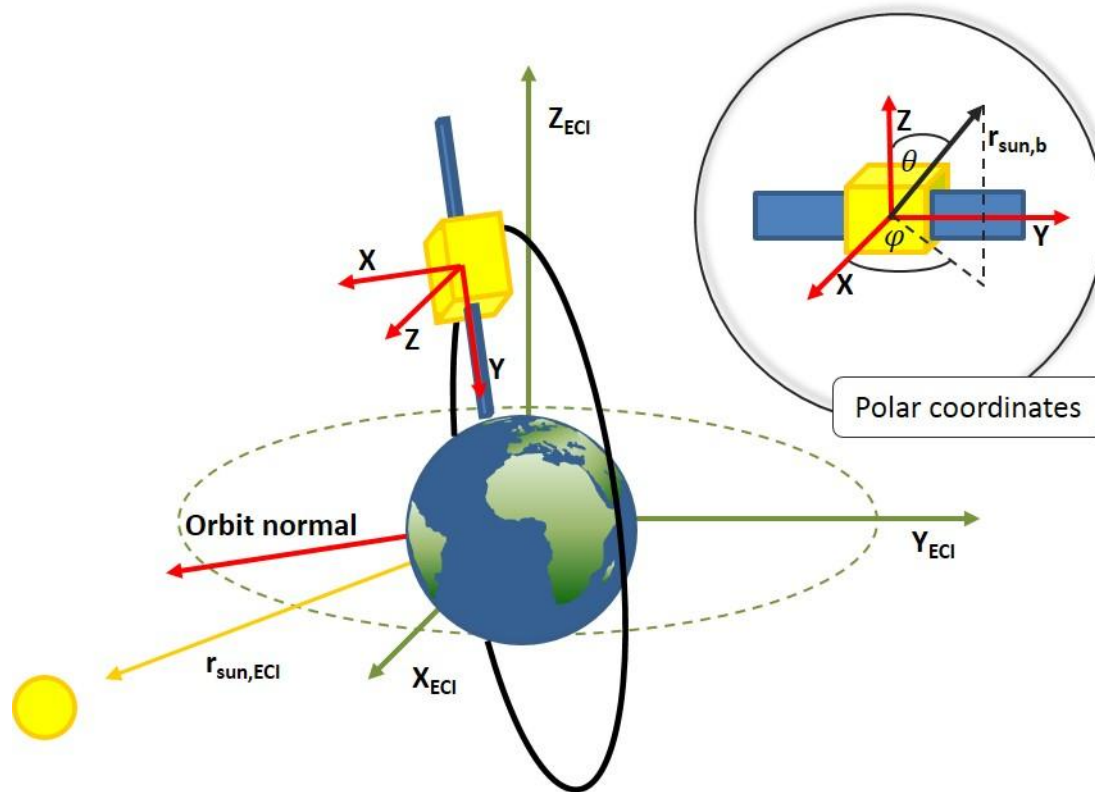
$$\mu_{SD}(t) = \frac{\gamma_{S,\text{BOL}}}{\gamma_{D,\text{BOL}}} e^{-\lambda t}$$

$$\gamma_S(t) = (1 - \alpha) \frac{\mu_{SD}(t)}{\mu_{SD,\text{BOL}} + 1} \qquad \gamma_D(t) = \frac{1 - \alpha}{1 + \mu_{SD}(t)}$$

# Contents

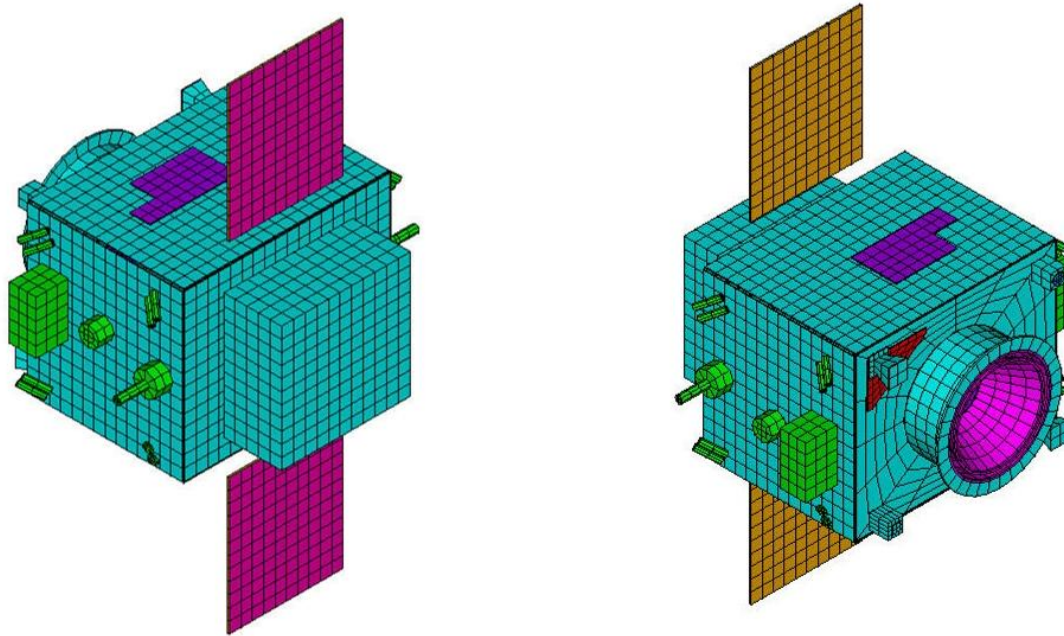
- ✓ Mission data analysis:  
Time-dependent frequency analysis by using wavelets
  
- ✓ **Modeling of non-gravitational disturbances**
  - ✓ Motivation
  - ✓ SRP/TRP modeling approach
  - ✓ **Example: MICROSCOPE**
  
- ✓ Outlook: post WEP test mission goals
  
- ✓ Conclusion

# MICROSCOPE: orbit



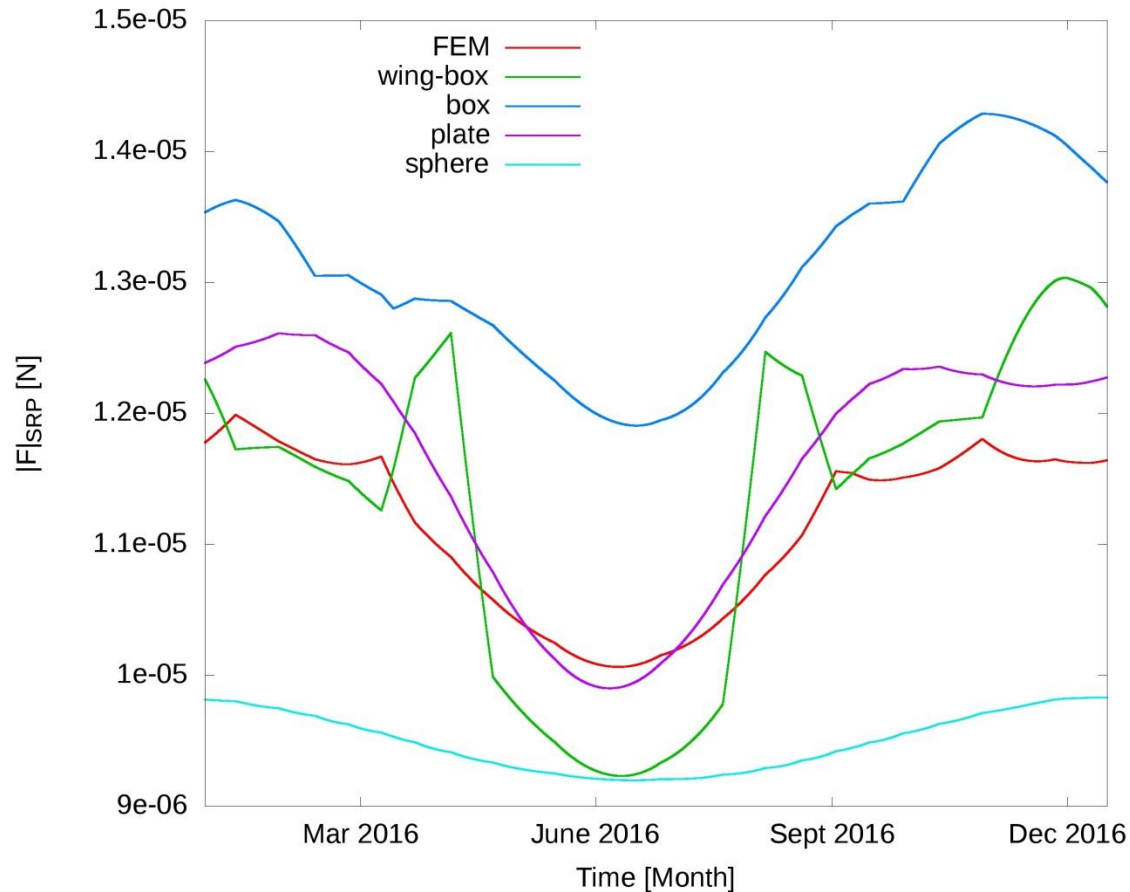
- ✓ MICROSCOPE orbit: altitude 710 km, circular and polar orbit (SSO)

# MICROSCOPE: detailed geometry model



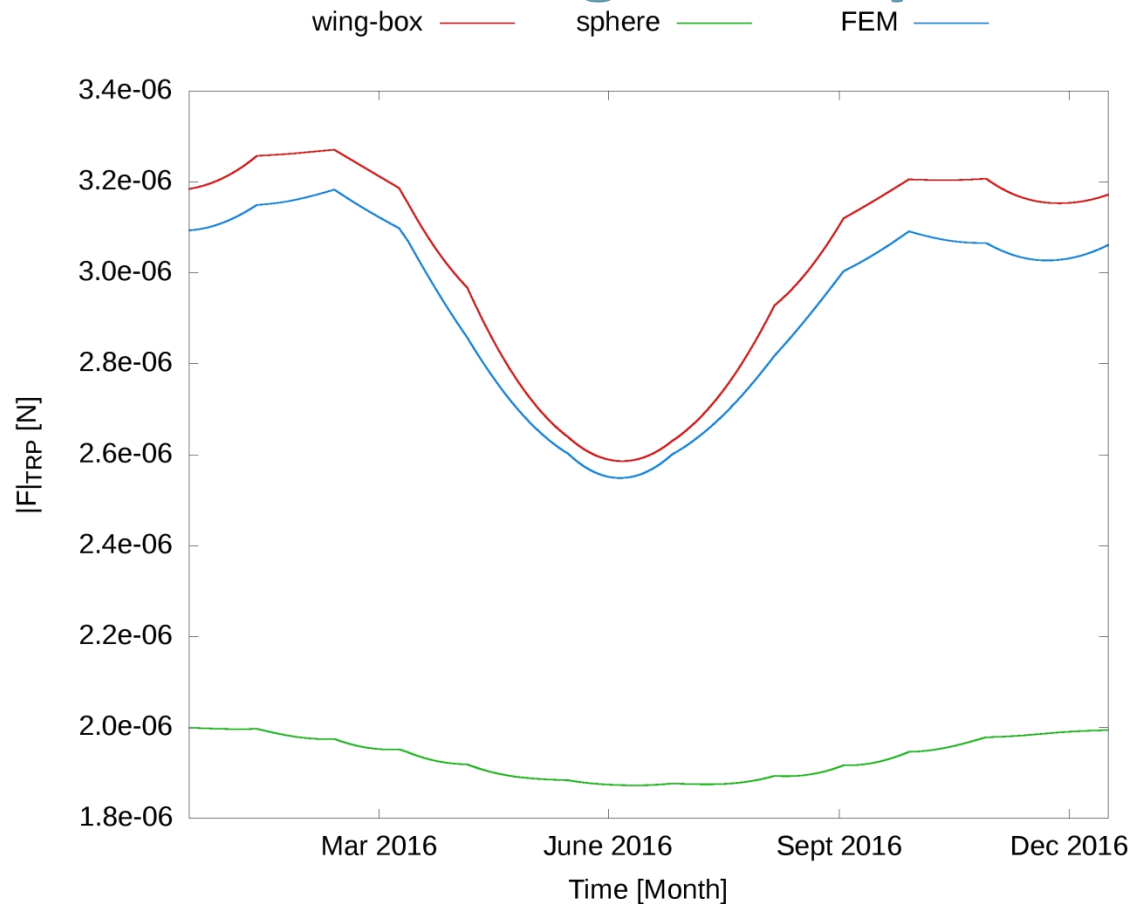
- MLI
- $Ant_e$  (Kevlar)
- $Ant_i$  (Kevlar, Composite)
- white coating
- Solar panel (front)
- Radiator surfaces
- Solar panel (rear face)

# SRP: influence of geometry models



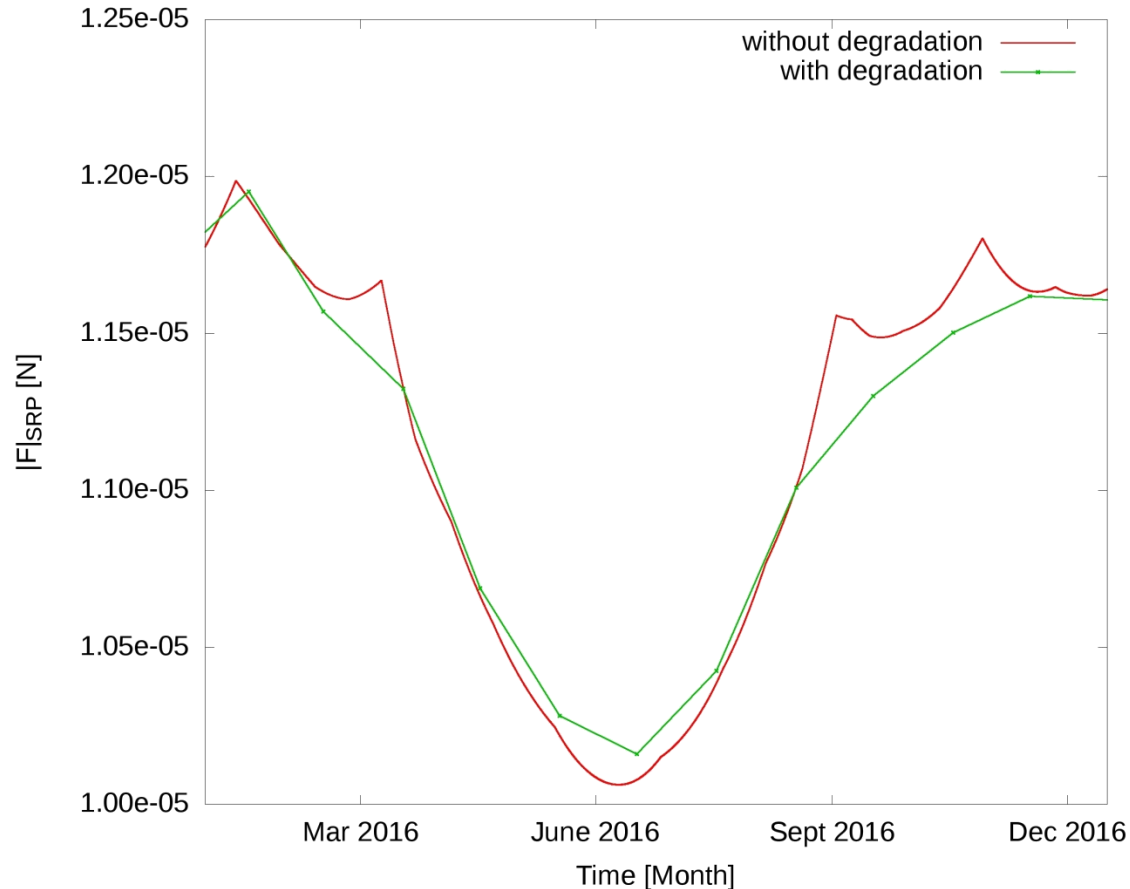
- ✓ Magnitude of the computed SRP force (simulated period of time: one year)
  - **different geometry models**, const. material coefficients for absorptivity and reflectivity, variation of angle between sun vector and orbit normal

# TRP: influence of geometry models



- ✓ Magnitude of the computed TRP force (simulated period of time: one year)
  - **different geometry models**, const. material coefficients for absorptivity and reflectivity, variation of angle between sun vector and orbit normal

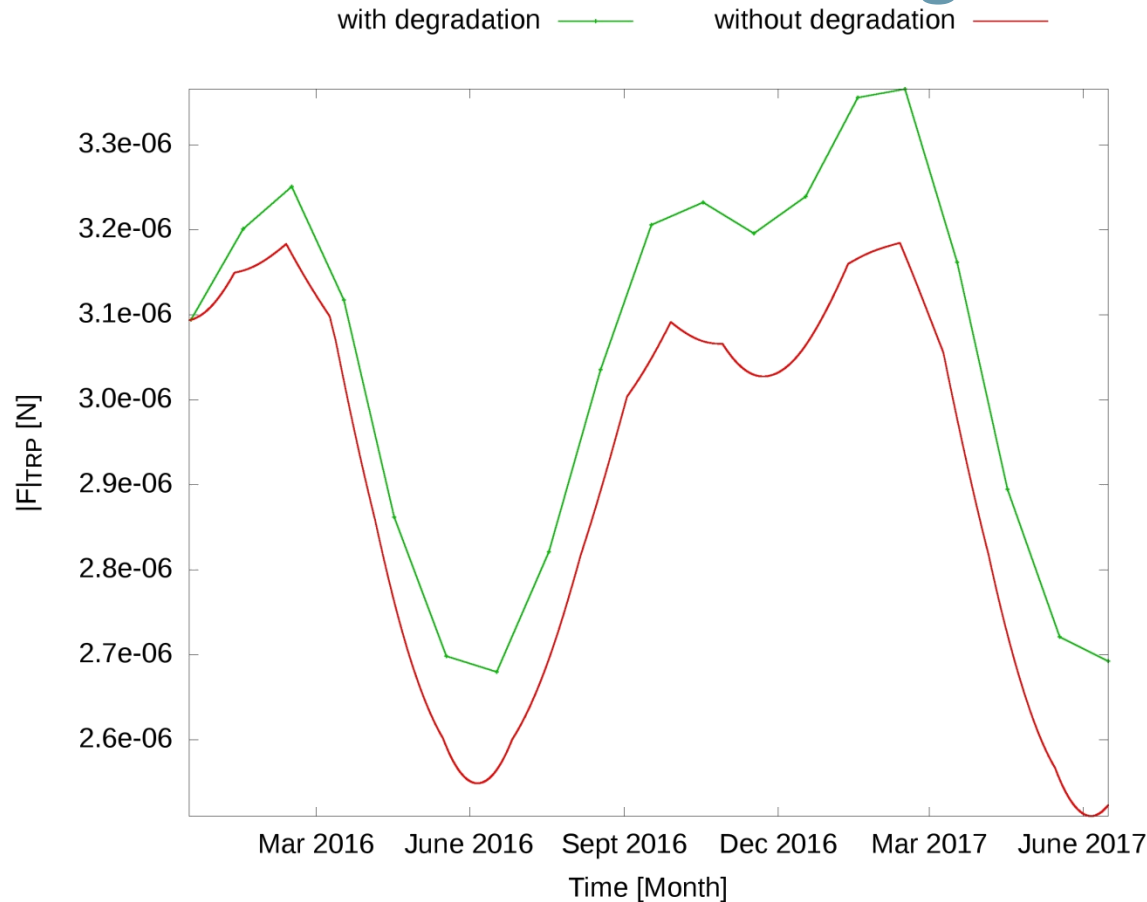
# SRP: influence of material degradation



- ✓ Magnitude of the computed SRP force (simulated period of time: one year)
  - detailed geometry model, **degradation of material properties** → **coefficients for absorptivity and reflectivity are time-dependent**, variation angle between sun vector and orbit normal



# TRP: influence of material degradation



- ✓ Magnitude of the computed TRP force (simulated period of time: one year)
  - detailed geometry model, **degradation of material properties** → **coefficients for absorptivity and reflectivity are time-dependent**, variation angle between sun vector and orbit normal

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- ✓ Mission data analysis:  
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# Outlook: post WEP test mission goals

- Data collection in most critical altitude range for spacecraft conjunction assessment and collision avoidance
- **Evaluation and improvement of existing thermosphere models**, e.g. NRLMSIS, JB2008
- **Improvement and evaluation of satellite non-gravitational force modeling** including disentanglement of different effects (SRP/TRP/drag etc.) by collecting unique data in non-drag-free mode
- Proposal for a technological experiment : CNES / TU Delft / ZARM
- SPP 1788 DynamicEarth

# Proposed mission details (measurement modes, duration, etc.)

- ✓ **Measurement without drag-free control**
    - Disturbances are directly visible in accelerometer axis
  - ✓ If possible **variation/modulation of pitch angles**
    - Changing cross-sectional drag surface
  - ✓ In addition **measurement during eclipse encounter**
    - Resolution of transient thermal effects and SRP evolution
- **As many orbits as feasible**
- **Optimal**: 1 year to cover seasonal effects

## Needed data, support

- ✓ Accelerometer data (MNOG/FRM) in non-drag free mode, full set of housekeeping data (→ N\_0 data sets)
- ✓ Operations by CNES
- ✓ Data evaluation and modeling: funding by national agencies

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# Conclusion

- ✓ ZARM data report: focusing on time-dependent frequency analysis based on wavelet analysis of the time signals
- ✓ With the help of standard cannonball and Box-And-Wing models it is not possible to diagnose and identify SRP/TRP disturbance effects with highest precision.
- ✓ Material degradation effects cannot be neglected for determining a complete “disturbance force and torque budget“
- ✓ Post mission goals: **measurement of non-gravitational forces** in non-drag free mode → new for field of research which has been nearly stagnant for decades

# Thank you for your attention.

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